

Théorie des goupilles de raquette**Théorie avancée des goupilles de raquette****Cas d'un glissement entre spirale et goupille**

Caractéristiques du spiral avec une spire externe semi-circulaire

➔ Référence : E:\Résonateur (TA)\Data\Bal_spiral plat (ex num).mcd(R)

Dimensions	$\epsilon p = 0.03 \text{ mm}$	$ha = 0.15 \text{ mm}$	$S = 4.5 \times 10^{-3} \text{ mm}^2$
$d2_{sp} = 4.52 \text{ mm}$	$d1_{sp} = 1.1 \text{ mm}$	$p_{sp} = 0.135 \text{ mm}$	$n_{sp} = 12.667$
$L_{sp} = 11.182 \text{ cm}$	$\psi_0 := 2 \cdot \pi \cdot n_{sp}$	$\psi_0 = 4.56 \times 10^3 \text{ deg}$	$E = 2.093 \times 10^{11} \text{ m}^{-2} \text{ N}$
Position du piton	$r_P := 0.5 \cdot d_{\text{piton}}$	$\alpha_P := 0$	$x_P := r_P \cdot \cos(\alpha_P) \quad y_P := r_P \cdot \sin(\alpha_P)$
	$x_P = 2.55 \text{ mm}$	$y_P = 0 \text{ mm}$	$z_P := x_P + i \cdot y_P$
Position du point d'attache à la virole	$r_V := 0.5 \cdot d1_{sp}$	$\alpha_V(\theta) := \psi_0 + \theta$	$x_V(\theta) := r_V \cdot \cos(\alpha_V(\theta)) \quad y_V(\theta) := r_V \cdot \sin(\alpha_V(\theta))$
Position du point de raccordement sur le spiral		$\alpha_A := 180 \cdot \text{deg}$	$r_A := 0.5 \cdot d2_{sp} \quad z_A := r_A \cdot e^{i \cdot \alpha_A}$
Spire externe formée d'un demi-cercle	$R_0 := r_P$	$x_{0t}(\alpha_t) := R_0 \cdot \cos(\alpha_t) \quad y_{0t}(\alpha_t) := R_0 \cdot \sin(\alpha_t) \quad z_{0t}(\alpha_t) := R_0 \cdot e^{i \cdot \alpha_t}$	
	$s_t(\alpha_t) := R_0 \cdot \alpha_t$	$l_t := s_t(\alpha_A)$	$l_t = 8.011 \text{ mm}$

Forme initiale du spiral

$$a := \frac{p_{sp}}{2 \cdot \pi} \quad r_s(\alpha) := r_A - a \cdot (\alpha - \alpha_A) \quad x_{0s}(\alpha) := r_s(\alpha) \cdot \cos(\alpha) \quad y_{0s}(\alpha) := r_s(\alpha) \cdot \sin(\alpha)$$

$$s_s(\alpha) := \frac{1}{2 \cdot a} \cdot (r_A^2 - r_s(\alpha)^2) \quad s_s(\alpha) := r_A \cdot (\alpha - \alpha_A) - \frac{a}{2} \cdot (\alpha - \alpha_A)^2 \quad L_t := s_s(\psi_0 + \alpha_A) + l_t$$

$$L_t = 11.983 \text{ cm}$$

Position angulaire des goupilles par rapport au piton:

$$\epsilon := 0.023 \quad s_g := \epsilon \cdot L_t \quad s_g = 2.756 \text{ mm} \quad \alpha_g := \frac{s_g}{R_0} \quad \alpha_g = 61.927 \text{ deg}$$

Amplitude stationnaire du balancier $\theta_0 = 270 \text{ deg}$

Position radiale de la goupille pour une élévation de contact donnée

Première approximation de la déformée de la spire externe entre piton et goupille $\theta_1 := 20 \cdot \text{deg}$

$$x_{0g}(\alpha_g) := R_0 \cdot \cos(\alpha_g) \quad y_{0g}(\alpha_g) := R_0 \cdot \sin(\alpha_g)$$

$$\xi_{0g}(\alpha_g) := \frac{R_0}{\alpha_g} \cdot \sin(\alpha_g) \quad \eta_{0g}(\alpha_g) := \frac{R_0}{\alpha_g} \cdot (1 - \cos(\alpha_g))$$

$$\beta := \arctan \left[\frac{-(x_{0g}(\alpha_g) - \xi_{0g}(\alpha_g))}{y_{0g}(\alpha_g) - \eta_{0g}(\alpha_g)} \right]$$

Jeu entre spiral et goupille au repos

$$j := \frac{\epsilon \cdot (y_{0g}(\alpha_g) - \eta_{0g}(\alpha_g))}{\cos(\beta)} \cdot \theta_1 \quad j = 0.011 \text{ mm}$$

Calcul de la matrice D_g

Calcul à partir de la première approximation de la déformée

$$z_{1t}(\theta, \alpha_t) := z_P + \frac{L_t \cdot R_0}{L_t + \theta \cdot R_0} \cdot \left(\exp\left(i \cdot \alpha_t \cdot \frac{L_t + \theta \cdot R_0}{L_t}\right) - 1 \right)$$

$$x_1(\theta, \alpha) := \operatorname{Re}(z_{1t}(\theta, \alpha)) \quad y_1(\theta, \alpha) := \operatorname{Im}(z_{1t}(\theta, \alpha)) \quad EI := E \cdot I_S \cdot N^{-1} \cdot m^{-2} \quad EI = 7.063 \times 10^{-8}$$

$$\xi_{1g}(\alpha_g) := \frac{1}{\alpha_g} \cdot \int_0^{\alpha_g} x_1(\theta_0, \alpha) d\alpha \quad \eta_{1g}(\alpha_g) := \frac{1}{\alpha_g} \cdot \int_0^{\alpha_g} y_1(\theta_0, \alpha) d\alpha$$

$$p_{21g}(\alpha_g) := \frac{1}{\alpha_g} \cdot \int_0^{\alpha_g} x_1(\theta_0, \alpha)^2 d\alpha \quad q_{21g}(\alpha_g) := \frac{1}{\alpha_g} \cdot \int_0^{\alpha_g} y_1(\theta_0, \alpha)^2 d\alpha$$

$$k_{1g}(\alpha_g) := \frac{1}{\alpha_g} \cdot \int_0^{\alpha_g} x_1(\theta_0, \alpha) \cdot y_1(\theta_0, \alpha) d\alpha$$

$$d_{111}(\alpha_g) := q_{21g}(\alpha_g) \cdot m^{-2} \quad d_{122}(\alpha_g) := p_{21g}(\alpha_g) \cdot m^{-2} \quad d_{133}(\alpha_g) := 1 \quad R_0 := R_0 \cdot m^{-1}$$

$$d_{112}(\alpha_g) := -k_{1g}(\alpha_g) \cdot m^{-2} \quad d_{113}(\alpha_g) := \eta_{1g}(\alpha_g) \cdot m^{-1} \quad d_{123}(\alpha_g) := -\xi_{1g}(\alpha_g) \cdot m^{-1}$$

$$D_{1g}(\alpha_g) := \frac{R_0 \cdot \alpha_g}{EI} \cdot \begin{pmatrix} d_{111}(\alpha_g) & d_{112}(\alpha_g) & d_{113}(\alpha_g) \\ d_{122}(\alpha_g) & d_{123}(\alpha_g) & 1 \\ d_{133}(\alpha_g) & d_{134}(\alpha_g) & 1 \end{pmatrix} \quad D_{1g}(\alpha_g) = \begin{pmatrix} 0.074 & -0.087 & 47.727 \\ -0.087 & 0.17 & -79.645 \\ 47.727 & -79.645 & 3.902 \times 10^4 \end{pmatrix}$$

Approximation à partir de la forme naturelle du spiral

$$p_{20g}(\alpha_g) := \frac{R_0^2}{2 \cdot \alpha_g} \cdot \left(\alpha_g + \frac{\sin(2 \cdot \alpha_g)}{2} \right) \quad q_{20g}(\alpha_g) := \frac{R_0^2}{2 \cdot \alpha_g} \cdot \left(\alpha_g - \frac{\sin(2 \cdot \alpha_g)}{2} \right) \quad k_{0g}(\alpha_g) := \frac{R_0^2}{2 \cdot \alpha_g} \cdot \sin(\alpha_g)^2$$

$$d_{11}(\alpha_g) := q_{20g}(\alpha_g) \cdot m^{-2} \quad d_{22}(\alpha_g) := p_{20g}(\alpha_g) \cdot m^{-2} \quad d_{33}(\alpha_g) := 1$$

$$d_{12}(\alpha_g) := -k_{0g}(\alpha_g) \cdot m^{-2} \quad d_{13}(\alpha_g) := \eta_{0g}(\alpha_g) \cdot m^{-1} \quad d_{23}(\alpha_g) := -\xi_{0g}(\alpha_g) \cdot m^{-1}$$

$$D_g(\alpha_g) := \frac{R_0 \cdot \alpha_g}{EI} \cdot \begin{pmatrix} d_{11}(\alpha_g) & d_{12}(\alpha_g) & d_{13}(\alpha_g) \\ d_{12}(\alpha_g) & d_{22}(\alpha_g) & d_{23}(\alpha_g) \\ d_{13}(\alpha_g) & d_{23}(\alpha_g) & 1 \end{pmatrix} \quad D_g(\alpha_g) = \begin{pmatrix} 0.078 & -0.091 & 48.738 \\ -0.091 & 0.176 & -81.231 \\ 48.738 & -81.231 & 3.902 \times 10^4 \end{pmatrix}$$

Calcul des formes quadratiques

$$\Delta(\alpha_g) := \sin(\alpha_g) \quad \gamma(\alpha_g) := \cos(\alpha_g) \quad x_{0g}(\alpha_g) := R_0 \cdot \cos(\alpha_g) \quad y_{0g}(\alpha_g) := R_0 \cdot \sin(\alpha_g)$$

$$H(\alpha_g) := \frac{R_0}{\alpha_g} \cdot (1 - \cos(\alpha_g)) \quad J(\alpha_g) := \frac{R_0}{\alpha_g} \cdot (\alpha_g - \sin(\alpha_g))$$

$$V_1(\alpha_g) := (\gamma(\alpha_g) \quad \Delta(\alpha_g) \quad 0)^T \quad V_2(\alpha_g) := (\Delta(\alpha_g) \quad -\gamma(\alpha_g) \quad -R_0)^T$$

$$W1_{g1}(\alpha_g) := \frac{1 \cdot s^2 \cdot kg^{-1}}{2} \cdot \mathbf{V}_1(\alpha_g)^T \cdot \mathbf{D}_{1g}(\alpha_g) \cdot \mathbf{V}_1(\alpha_g)$$

$$W1_{g1}(\alpha_g) = 0.038 \text{ kg}^{-1} \cdot s^2$$

$$W_{g1}(\alpha_g) := \frac{R_0^3}{4 \cdot E \cdot I_s} \cdot (\alpha_g - \sin(\alpha_g) \cdot \cos(\alpha_g))$$

$$W_{g1}(\alpha_g) = 0.039 \text{ kg}^{-1} \cdot s^2$$

$$W1_{g2}(\alpha_g) := \frac{1 \cdot s^2 \cdot kg^{-1}}{2} \cdot \mathbf{V}_2(\alpha_g)^T \cdot \mathbf{D}_{1g}(\alpha_g) \cdot \mathbf{V}_2(\alpha_g)$$

$$W1_{g2}(\alpha_g) = 7.809 \times 10^{-3} \text{ kg}^{-1} \cdot s^2$$

$$W_{g2}(\alpha_g) := \frac{R_0^3}{4 \cdot E \cdot I_s} \cdot [3 \cdot \alpha_g + \sin(\alpha_g) \cdot (\cos(\alpha_g) - 4)]$$

$$W_{g2}(\alpha_g) = 7.531 \times 10^{-3} \text{ kg}^{-1} \cdot s^2$$

$$W1_{g3}(\alpha_g) := \frac{1 \cdot s^2 \cdot kg^{-1}}{2} \cdot \mathbf{V}_1(\alpha_g)^T \cdot \mathbf{D}_{1g}(\alpha_g) \cdot \mathbf{V}_2(\alpha_g)$$

$$W1_{g3}(\alpha_g) = 0.017 \text{ kg}^{-1} \cdot s^2$$

$$W_{g3}(\alpha_g) := \frac{R_0^3}{4 \cdot E \cdot I_s} \cdot (1 - \cos(\alpha_g))^2$$

$$W_{g3}(\alpha_g) = 0.016 \text{ kg}^{-1} \cdot s^2$$

$$\mathbf{V}_g(\alpha_g) := (R_0 \cdot \sin(\alpha_g) \quad -R_0 \cdot \cos(\alpha_g) \quad 1)^T$$

$$W1_{c2}(\alpha_g) := \frac{1 \cdot kg \cdot m^2 \cdot s^{-2}}{2} \cdot ((\mathbf{V}_g(\alpha_g)))^T \cdot \mathbf{D}_{1g}(\alpha_g)^{-1} \cdot \mathbf{V}_g(\alpha_g)$$

$$W1_{c2}(\alpha_g) = 6.41 \times 10^{-5} \text{ m}^2 \cdot kg \cdot s^{-2}$$

$$\Delta_g(\alpha_g) := \frac{R_0^4}{4 \cdot \alpha_g^3} \cdot (\alpha_g - \sin(\alpha_g)) \cdot [\alpha_g \cdot (\alpha_g + \sin(\alpha_g)) - 4 \cdot (1 - \cos(\alpha_g))]$$

$$\Delta_g(\alpha_g) = 7.057 \times 10^{-3} \text{ mm}^4$$

$$W_{c2}(\alpha_g) := \frac{E \cdot I_s \cdot R_0^3}{8 \cdot \Delta_g(\alpha_g) \cdot \alpha_g^3} \cdot [3 \cdot \alpha_g^2 - 2 \cdot \alpha_g \cdot \sin(\alpha_g) \cdot (2 + \cos(\alpha_g)) - (1 - \cos(\alpha_g)) \cdot (1 - 7 \cdot \cos(\alpha_g))]$$

$$W_{c2}(\alpha_g) = 1.127 \times 10^{-4} \text{ m}^2 \cdot kg \cdot s^{-2}$$

Coefficient de frottement limite

$$F1(\alpha_g) := \frac{H(\alpha_g) \cdot W1_{g3}(\alpha_g) - J(\alpha_g) \cdot W1_{g1}(\alpha_g)}{H(\alpha_g) \cdot W1_{g2}(\alpha_g) - J(\alpha_g) \cdot W1_{g3}(\alpha_g)}$$

$$F1(\alpha_g) = 1.645$$

$$F(\alpha_g) := \frac{H(\alpha_g) \cdot W_{g3}(\alpha_g) - J(\alpha_g) \cdot W_{g1}(\alpha_g)}{H(\alpha_g) \cdot W_{g2}(\alpha_g) - J(\alpha_g) \cdot W_{g3}(\alpha_g)}$$

$$F(\alpha_g) = 1.322$$

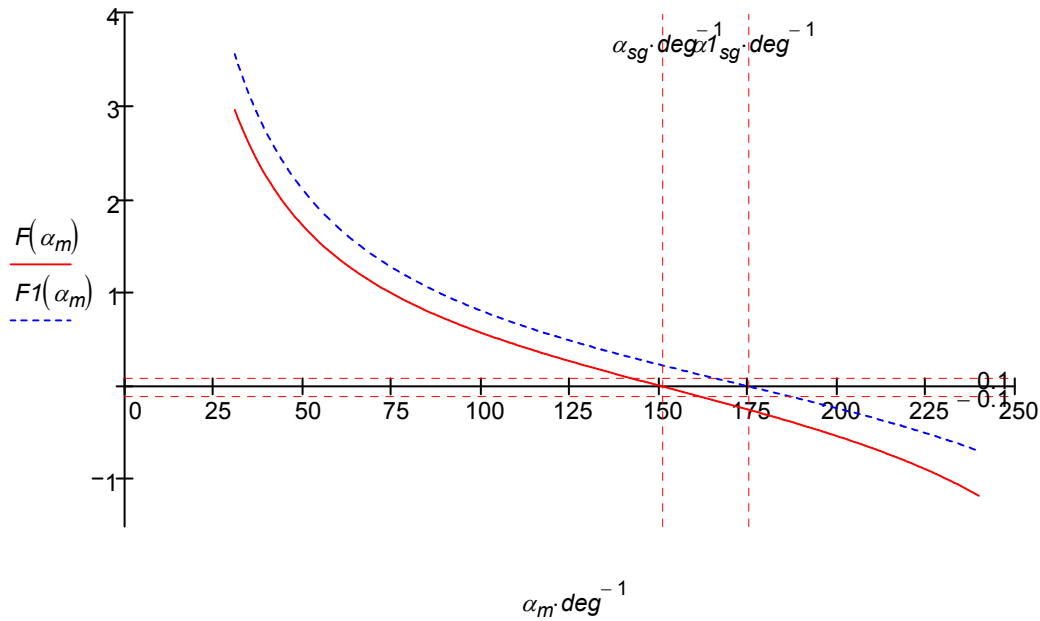
$$F(\alpha_g) := \frac{-\alpha_g^2 + \alpha_g \cdot \sin(\alpha_g) \cdot (1 + \cos(\alpha_g)) + (1 - \cos(\alpha_g)) \cdot (1 - 3 \cdot \cos(\alpha_g))}{(1 - \cos(\alpha_g)) \cdot [(2 + \cos(\alpha_g)) \cdot \alpha_g - 3 \cdot \sin(\alpha_g)]}$$

$$F(\alpha_g) = 1.322$$

$$\alpha_{sg} := 151 \cdot \text{deg} \quad \alpha_{sg} := \text{racine}(F(\alpha_{sg}), \alpha_{sg}) \quad \alpha_{sg} = 151.277 \text{ deg}$$

$$\alpha1_{sg} := 175 \cdot \text{deg} \quad \alpha1_{sg} := \text{racine}(F(\alpha1_{sg}), \alpha1_{sg}) \quad \alpha1_{sg} = 175.718 \text{ deg}$$

$$\alpha_m := 31 \cdot \text{deg}, 32 \cdot \text{deg} \dots 240 \cdot \text{deg}$$



Réaction normale à la goupille

Coefficient de frottement $f_g := 0.1$ $\mu_g := f_g$

$$F1_{gn}(\theta, \alpha_g) := \frac{\varepsilon \cdot H(\alpha_g) \cdot (\theta - \theta_1)}{2 \cdot (W1_{g1}(\alpha_g) - \mu_g \cdot W1_{g3}(\alpha_g))} \quad F1_{gn}(\theta_0, \alpha_g) = 1.709 \times 10^{-3} \text{ N}$$

$$F_{gn}(\theta, \alpha_g) := \varepsilon \cdot (\theta - \theta_1) \cdot \frac{2 \cdot E \cdot I_s}{R_0^2} \cdot \frac{1 - \cos(\alpha_g)}{\alpha_g \cdot [\alpha_g - \sin(\alpha_g) \cdot \cos(\alpha_g) - \mu_g \cdot (1 - \cos(\alpha_g))^2]} \quad F_{gn}(\theta_0, \alpha_g) = 1.675 \times 10^{-3} \text{ N}$$

Calcul du glissement

$$q1(\alpha_g) := \frac{W1_{g1}(\alpha_g)}{W1_{g3}(\alpha_g)} \quad \Delta s_{1g}(\theta, \theta_1, \alpha_g, f_g) := \varepsilon \cdot (\theta - \theta_1) \cdot \frac{F(\alpha_g) - \mu_g}{q1(\alpha_g) - \mu_g} \cdot \frac{J(\alpha_g) \cdot W1_{g3}(\alpha_g) - H(\alpha_g) \cdot W1_{g2}(\alpha_g)}{W1_{g3}(\alpha_g)}$$

$$\Delta s_g(\theta, \theta_1, \alpha_g, f_g) := -\varepsilon \cdot (\theta - \theta_1) \cdot R_0 \cdot \frac{(1 - \cos(\alpha_g)) \cdot [(2 + \cos(\alpha_g)) \cdot \alpha_g - 3 \cdot \sin(\alpha_g)]}{\alpha_g \cdot [\alpha_g - \sin(\alpha_g) \cdot \cos(\alpha_g) - f_g \cdot (1 - \cos(\alpha_g))^2]} \cdot (F(\alpha_g) - f_g)$$

$$\Delta s_{1g}(\theta_0, \theta_1, \alpha_g, f_g) = -6.247 \times 10^{-3} \text{ mm} \quad \Delta s_g(\theta_0, \theta_1, \alpha_g, f_g) = -5.583 \times 10^{-3} \text{ mm}$$

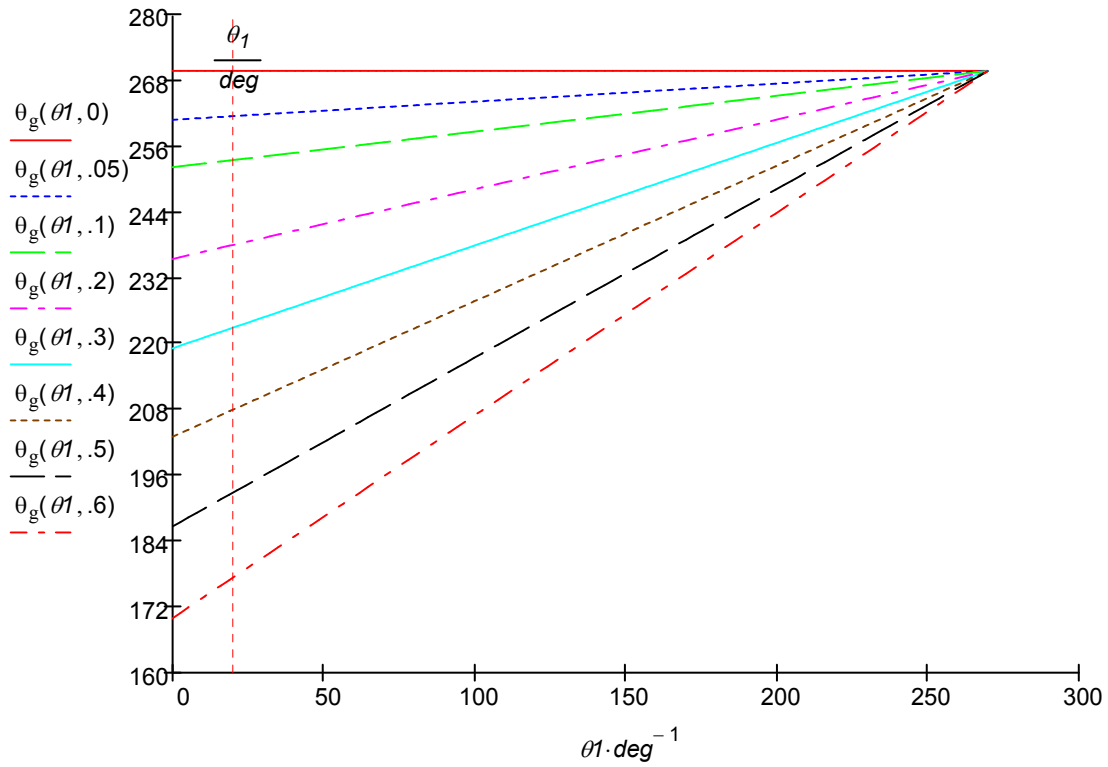
Remarque Les erreurs étant relativement faibles pour un angle α_g inférieur à 90° , nous continuerons les calculs en ne considérant que les valeurs obtenues à partir de la forme naturelle du spiral

Evolution du glissement en fonction de l'élongation du balancier

Angle de début de glissement inverse

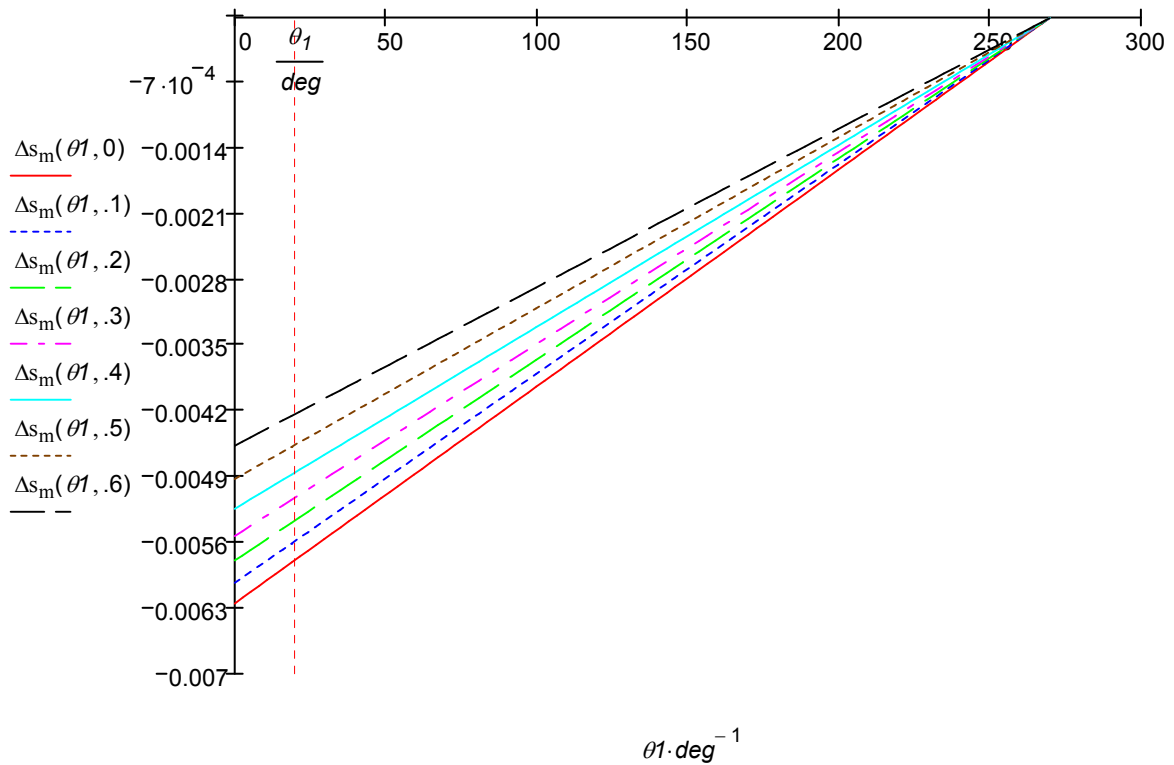
$$q(\alpha_g) := \frac{\alpha_g - \sin(\alpha_g) \cdot \cos(\alpha_g)}{(1 - \cos(\alpha_g))^2} \quad \theta_g(\theta_0, \theta_1, \alpha_g, f_g) := \frac{q(\alpha_g) + f_g}{F(\alpha_g) + f_g} \cdot \frac{F(\alpha_g) - f_g}{q(\alpha_g) - f_g} \cdot (\theta_0 - \theta_1) + \theta_1$$

$$\theta_1 := 0, 0.01 \cdot \theta_0 \dots \theta_0 \quad \theta_g(\theta_1, f_g) := \theta_g(\theta_0, \theta_1, \alpha_g, f_g) \cdot \text{deg}^{-1} \quad \theta_g(\theta_0, \theta_1, \alpha_g, f_g) = 253.7 \text{ deg}$$



Glissement maximum

$$\Delta s_m(\theta_1, f_g) := \Delta s_g(\theta_0, \theta_1, \alpha_g, f_g) \quad \Delta s_m(\theta_1, f_g) := \Delta s_m(\theta_1, f_g) \cdot \text{mm}^{-1}$$



Glissement inverse

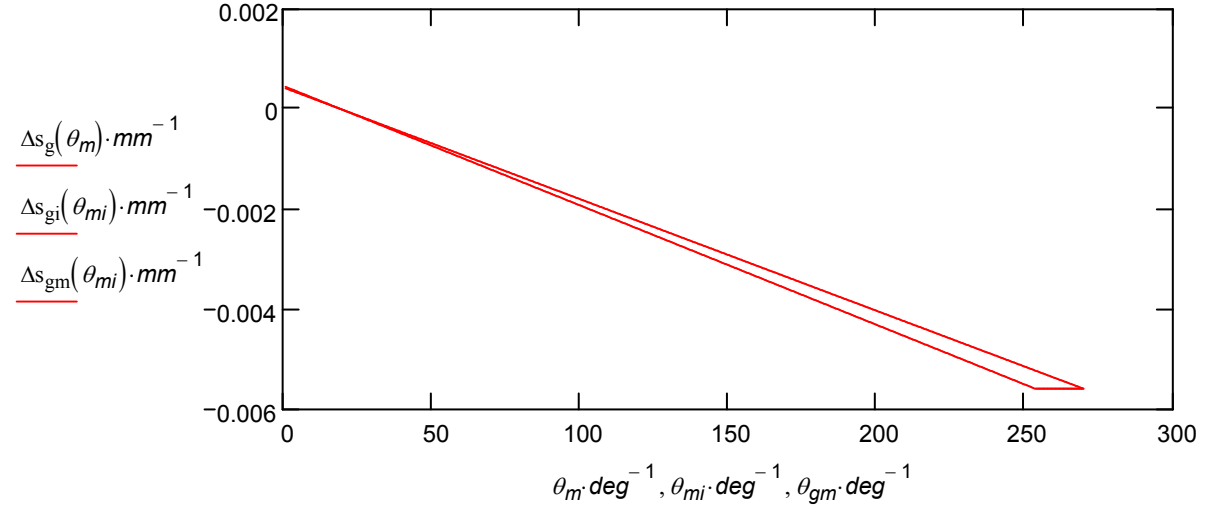
$$\Delta s_{gi}(\theta, \theta_1, \alpha_g, f_g) := -\varepsilon \cdot (\theta - \theta_1) \cdot R_0 \cdot \frac{(1 - \cos(\alpha_g)) \cdot [(2 + \cos(\alpha_g)) \cdot \alpha_g - 3 \cdot \sin(\alpha_g)]}{\alpha_g \cdot [\alpha_g - \sin(\alpha_g) \cdot \cos(\alpha_g) + f_g \cdot (1 - \cos(\alpha_g))^2]} \cdot (F(\alpha_g) + f_g)$$

Graphes de l'évolution du glissement en fonction de l'élongation du balancier

$$\Delta s_g(\theta) := \Delta s_g(\theta, \theta_1, \alpha_g, f_g) \quad \theta_m := 1 \cdot \text{deg}, 1.5 \cdot \text{deg} \dots \theta_0$$

$$\Delta s_{gi}(\theta) := \Delta s_{gi}(\theta, \theta_1, \alpha_g, f_g) \quad \theta_{mi} := 1 \cdot \text{deg}, 1.5 \cdot \text{deg} \dots \theta_g(\theta_0, \theta_1, \alpha_g, f_g)$$

$$\Delta s_{gm}(\theta) := \Delta s_g(\theta_0, \theta_1, \alpha_g, f_g) \quad \theta_{gm} := \theta_g(\theta_0, \theta_1, \alpha_g, f_g), \theta_g(\theta_0, \theta_1, \alpha_g, f_g) + 0.2 \cdot \text{deg} \dots \theta_0$$



Accroissement de l'angle polaire de la tangente au spiral au point de contact

$$N(\alpha_g) := \frac{E \cdot I_s}{2 \cdot R_0 \cdot \alpha_g \cdot W_{c2}(\alpha_g)} \quad N(\alpha_g) = 0.114$$

$$M_g(\alpha_g) := \mathbf{D}_g(\alpha_g)^{-1} \cdot \begin{pmatrix} y_{0g}(\alpha_g) \cdot m^{-1} \\ -x_{0g}(\alpha_g) \cdot m^{-1} \\ 1 \end{pmatrix} \quad m_g(\alpha_g) := M_g(\alpha_g)_0 \cdot N \quad n_g(\alpha_g) := M_g(\alpha_g)_1 \cdot N$$

$$\varphi_{sg}(\theta, \theta_1, \alpha_g, f_g) := \varepsilon \cdot (\theta - \theta_1) \cdot (N(\alpha_g) - 1) - \frac{\Delta s_g(\theta, \theta_1, \alpha_g, f_g)}{2 \cdot W_{c2}(\alpha_g)} \cdot (n_g(\alpha_g) \cdot \gamma(\alpha_g) - m_g(\alpha_g) \cdot \Delta(\alpha_g))$$

$$\varphi_{sg}(\theta_0, \theta_1, \alpha_g, f_g) = -4.502 \text{ deg} \quad \Delta \varphi_g := \varphi_{sg}(\theta_0, \theta_1, \alpha_g, f_g) + \varepsilon \cdot (\theta_0 - \theta_1)$$

Sans goupille $\Delta \varphi := \theta_0 \cdot \frac{R_0 \cdot \alpha_g}{L_t} \quad \Delta \varphi = 6.21 \text{ deg} \quad \Delta \varphi_g = 1.248 \text{ deg}$

Perturbation de marche dans le cas de deux goupilles

$$\phi_1(\theta_1, \theta_0) := \arcsin\left(\frac{\theta_1}{\theta_0}\right) \cdot (-\theta_0 \leq \theta_1 \leq \theta_0) + \frac{\pi}{2} \cdot (\theta_1 > \theta_0) - \frac{\pi}{2} \cdot (\theta_1 < -\theta_0)$$

$$\phi_2(\theta_2, \theta_0) := -\arcsin\left(\frac{\theta_2}{\theta_0}\right) \cdot (-\theta_0 \leq \theta_2 \leq \theta_0) + \frac{\pi}{2} \cdot (\theta_2 < -\theta_0) - \frac{\pi}{2} \cdot (\theta_2 > \theta_0)$$

$$\delta_1(\theta_1, \theta_0) := \frac{-\varepsilon}{4 \cdot \pi} \cdot (\pi - 2 \cdot \phi_1(\theta_1, \theta_0) - \sin(2 \cdot \phi_1(\theta_1, \theta_0)))$$

$$\delta_2(\theta_2, \theta_0) := \frac{-\varepsilon}{4 \cdot \pi} \cdot (\pi - 2 \cdot \phi_2(\theta_2, \theta_0) - \sin(2 \cdot \phi_2(\theta_2, \theta_0)))$$

Spiral à égales distances des goupilles en position d'équilibre:

$$\theta_2 := -\theta_1$$

Théorie élémentaire

$$\delta_1(\theta_1, \theta_0) = -5.208 \times 10^{-3} \quad \delta_2(\theta_2, \theta_0) = -5.208 \times 10^{-3} \quad \phi_1(\theta_1, \theta_0) = 0.074 \quad \phi_2(\theta_2, \theta_0) = 0.074$$

$$\mu_{\text{él}}(\theta_0) := -86400 \cdot (\delta_1(\theta_1, \theta_0) + \delta_2(\theta_2, \theta_0)) \quad \mu_{\text{él}}(\theta_0) = 899.975$$

Théorie avancée

$$M'(\alpha_g) := \frac{[\alpha_g \cdot (2 + \cos(\alpha_g)) - 3 \cdot \sin(\alpha_g)] \cdot [\alpha_g^2 - \alpha_g \cdot \sin(\alpha_g) \cdot (1 + \cos(\alpha_g)) - (1 - \cos(\alpha_g)) \cdot (1 - 3 \cdot \cos(\alpha_g))]}{\alpha_g \cdot (1 - \cos(\alpha_g)) \cdot [3 \cdot \alpha_g^2 - 2 \cdot \alpha_g \cdot \sin(\alpha_g) \cdot (2 + \cos(\alpha_g)) - (1 - \cos(\alpha_g)) \cdot (1 - 7 \cdot \cos(\alpha_g))]}$$

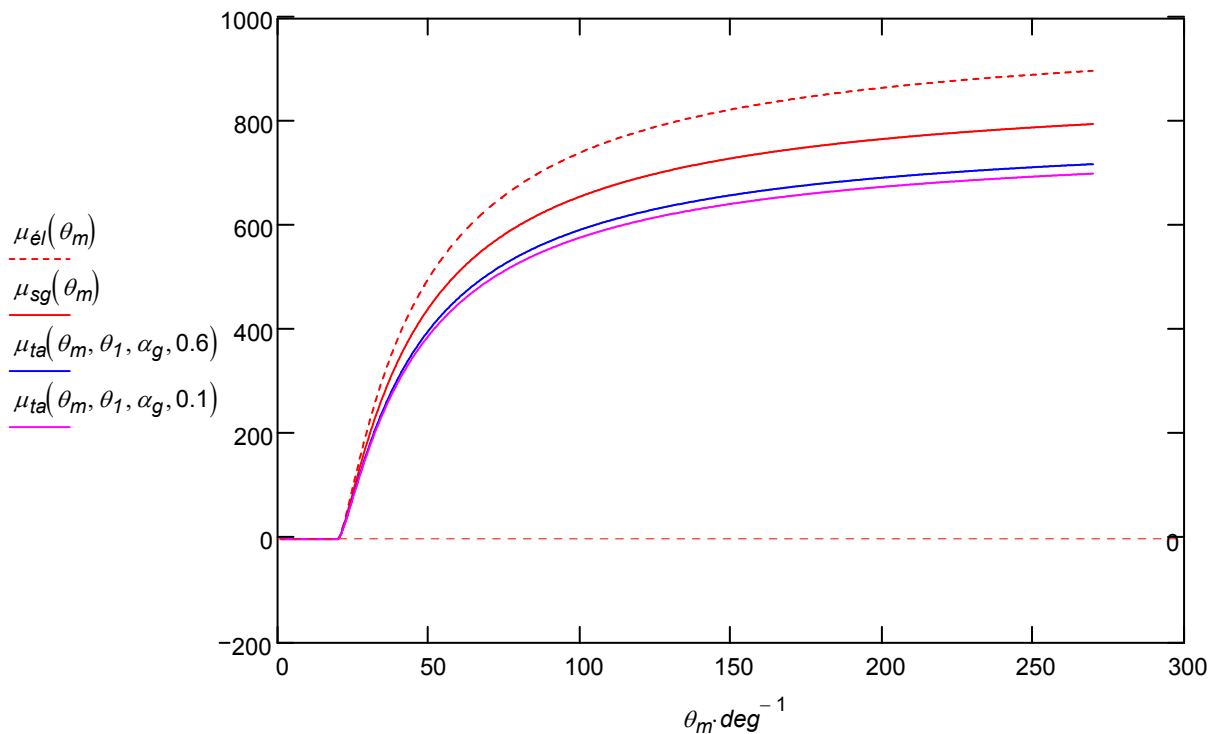
$$\phi_g(\theta_0, \theta_1, \alpha_g, f_g) := \arcsin \left[\sin(\phi_1(\theta_1, \theta_0)) + \frac{F(\alpha_g) - f_g}{q(\alpha_g) - f_g} \cdot \frac{q(\alpha_g) + f_g}{F(\alpha_g) + f_g} \cdot (1 - \sin(\phi_1(\theta_1, \theta_0))) \right]$$

$$\delta_g(\theta_0, \theta_1, \alpha_g, f_g) := \frac{\varepsilon}{4 \cdot \pi} \cdot (\pi - 2 \cdot \phi_g(\theta_0, \theta_1, \alpha_g, f_g) - \sin(2 \cdot \phi_g(\theta_0, \theta_1, \alpha_g, f_g)))$$

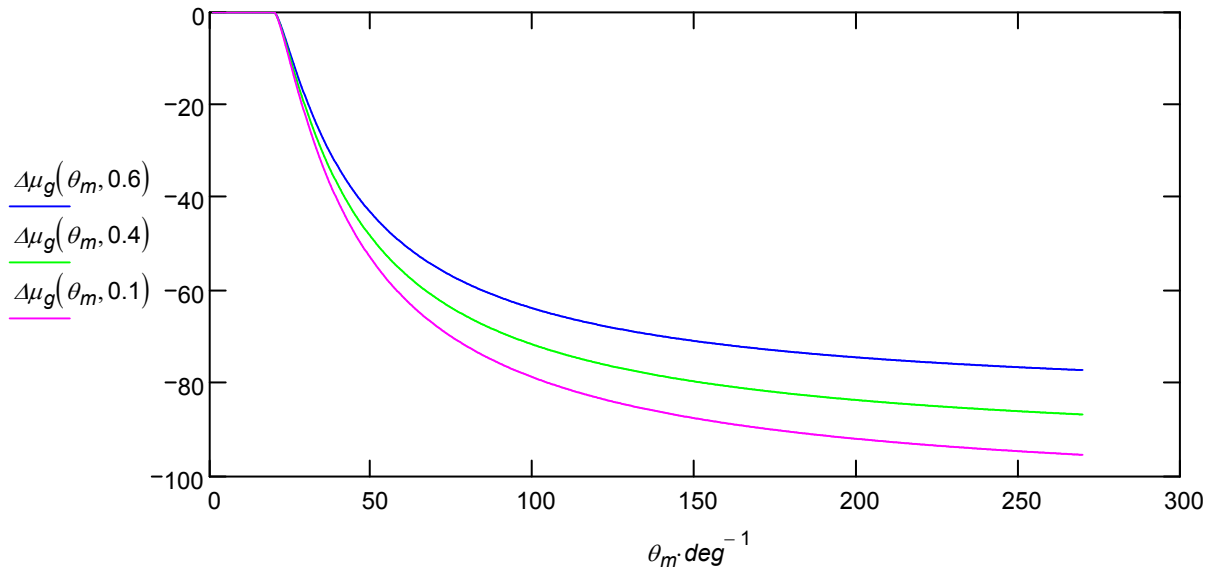
$$K_1(\alpha_g, f_g) := (1 - N(\alpha_g)) + M'(\alpha_g) \cdot \left(\frac{F(\alpha_g) - f_g}{q(\alpha_g) - f_g} + \frac{F(\alpha_g) + f_g}{q(\alpha_g) + f_g} \right) \quad K_2(\alpha_g, f_g) := M'(\alpha_g) \cdot \frac{F(\alpha_g) + f_g}{q(\alpha_g) + f_g}$$

$$\mu_{\text{ta}}(\theta_0, \theta_1, \alpha_g, f_g) := -86400 \cdot 2 \cdot (K_1(\alpha_g, f_g) \cdot \delta_1(\theta_1, \theta_0) + K_2(\alpha_g, f_g) \cdot \delta_g(\theta_0, \theta_1, \alpha_g, f_g))$$

$$\mu_{\text{sg}}(\theta_0) := \mu_{\text{él}}(\theta_0) \cdot (1 - N(\alpha_g)) \quad \text{marche en cas de glissement impossible}$$



$$\Delta\mu_g(\theta_0, f_g) := \mu_{ta}(\theta_0, \theta_1, \alpha_g, f_g) - \mu_{sg}(\theta_0)$$



Réglage par la raquette

$$\delta_1(\theta_1, \theta_0, \alpha_g) := \frac{-R_0 \cdot \alpha_g}{4 \cdot \pi \cdot L_t} \cdot (\pi - 2 \cdot \phi_1(\theta_1, \theta_0) - \sin(2 \cdot \phi_1(\theta_1, \theta_0)))$$

$$\delta_g(\theta_0, \theta_1, \alpha_g, f_g) := \frac{R_0 \cdot \alpha_g}{4 \cdot \pi \cdot L_t} \cdot (\pi - 2 \cdot \phi_g(\theta_0, \theta_1, \alpha_g, f_g) - \sin(2 \cdot \phi_g(\theta_0, \theta_1, \alpha_g, f_g)))$$

$$\mu_{ta}(\theta_1, \theta_0, \alpha_g, f_g) := -86400 \cdot 2 \cdot (K_1(\alpha_g, f_g) \cdot \delta_1(\theta_1, \theta_0, \alpha_g) + K_2(\alpha_g, f_g) \cdot \delta_g(\theta_0, \theta_1, \alpha_g, f_g))$$

$$\alpha_m := 40 \cdot \text{deg}, 42 \cdot \text{deg} \dots 90 \cdot \text{deg}$$

